## SPE 168278-MS <br> Optimizing Horizontal Wellbore Design to Extend Reach with Coiled Tubing

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## Introduction

- What?
- How can wellbore designs be altered to maximize coil tubing reach capacity?
- Concentrate on key wellbore variables that effect coil tubing lockup depths
- Maintain a set of control variables
- Compare field data to model results
- Provide a set of recommendations for drilling of wells
- Why?
- Allow for wellbore cleanouts post frac
- Allow all frac stages to be stimulated
- Prevent sterilizing production and reserves due to inability to reach TD


## Background

- Area of interest:
- Western Canada, Montney Formation
- Investigation drivers:
- CT annular frac design
- Wellbore interventions
- General:
- Wellbore lengths
- \# of stimulations
- Trends


Western Canada - Horizontal Well Statistics1


1. Canadian Discovery, Western Canadian Frac Database

## Horizontal Wellbore Design Factors

- Build Rate
- Expected to have largest impact
- Turn Rate
- Multi-well pad applications
- Casing Size
- Cost
- Artificial Lift



## Horizontal Wellbore Design

## Limiting Factors

- Directional tools
- Geology
- Surface access
- Stimulation System
- Economics


Fox Creek, Alberta

2014

## Coil Tubing Model Design

## Manipulated Variables

- Build Rate
- $\mathbf{0 - 2 0} 0^{\circ} / \mathbf{3 0} \mathbf{m}$
- Turn Rate
- $0-6^{\circ} / 30 \mathrm{~m}$
- 'Build and turn'

- Casing Size
- 114 mm
- 139 mm
- 139 mm w/ 114 mm lateral



## Coil Tubing Model Assumptions

\(\left.$$
\begin{array}{|lccc|}\hline \text { Variable } & \text { Assumed Value } & \text { Justification } \\
\hline \text { Coil tubing OD } & 50.8 \mathrm{~mm} & 2^{\prime \prime} & \begin{array}{c}\text { Match field data } \\
\text { Common size } \\
\text { Annular velocity limits }\end{array}
$$ <br>
\hline TVD \& 2000 \mathrm{~m} \& 6561 \mathrm{ft} \& Match field data <br>
\hline Friction Coefficient \& 0.3 \& Conservative value used <br>
\hline Lateral \& Smooth / Flat \& Impractical to model random <br>

variations\end{array}\right]\)| Fresh Water |
| :--- |

## Results - Build Angle


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Note: Y-axis depicts percentage change in lateral length relative to an $8^{\circ} / 30 \mathrm{~m}$ build rate

## Results - Turn Angle



## 

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## Results - Casing Size

## Change in Percent Lateral (\%) vs Build Angles (114 mm casing)



Change in Percent Lateral (\%) vs Build Angles (139 mm casing)


## Results - Sinusoidal and Helical Buckling



Sinusoidal Bucking and Helical Buckling (114 mm casing)

* 0 degree turn $(\operatorname{Sin}) ~ 2$ degree turn (sin)
$\longleftarrow 4$ degree turn $(\sin ) ~ \longleftarrow 6$ degree turn $(\sin )$
$\cdots$ turn (sin)



## COILED TUBING \& WELL ITTERVEATION

conference o ehtibition

## Matching Field Data



## Quantifying Model to Field Data

- 30 well data set
- Compare matched friction coefficient
- Large variety of well types
- Casing size ignored (proven to be lower impact variable)
- Build to 45 - turn @ $4^{\circ} / 30 \mathrm{~m}$

| Average <br> build <br> (degrees <br> $/ 30 \mathrm{~m})$ | Build- <br> Land | Build- <br> land- <br> turn | Build to 45 <br> deg - start <br> turn |
| :---: | :---: | :---: | :---: |
| $\mathbf{4}$ | - | - | 0.150 |
| $\mathbf{5}$ | 0.300 | - | 0.247 |
| $\mathbf{6}$ | 0.300 | 0.270 | 0.263 |
| $\mathbf{7}$ | 0.300 | 0.213 | 0.260 |
| $\mathbf{8}$ | 0.300 | - | 0.225 | shown to be lowest average friction coefficient

## Conclusions



Build rates of $4^{\circ} / 30 \mathrm{~m}$


Turn rates of $2-3^{\circ} / 30 \mathrm{~m}$ 'Build and turn'


114 mm monobore design

2014

## Thank You / Questions

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